

# Controlling wettability through modeling-based surface topography engineering

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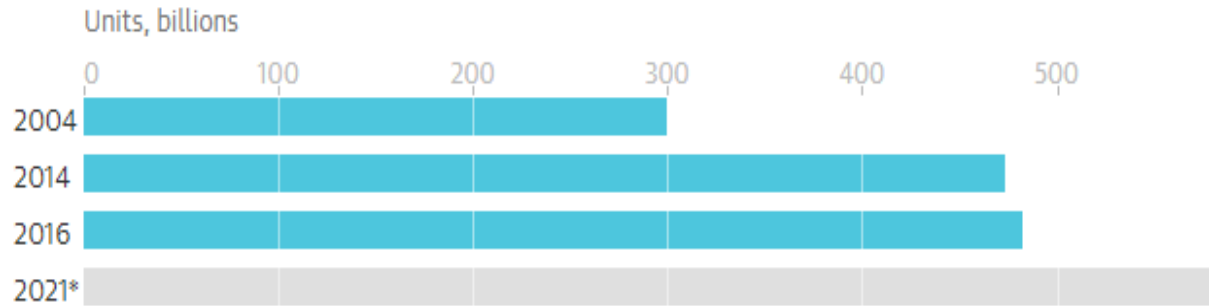


- 1 Problematic & Motivation**
- 2 Proposed solution**
- 3 Solution implementation**
- 4 Solution validation**
- 5 Conclusions & remarks**

# Problematic & Motivation

□ **Surface wetting** was identified as the prevalent mechanism related to adhesion of a liquid onto a solid surface

Global PET plastic bottle production



Guardian graphic | Source: Euromonitor. \* forecast

More than **480bn** plastic bottles were made in 2016

By 2021 demand will climb up to **~580bn**

Equivalent to 1M/min or 17k/s

If placed end-to-end, they extend **more than halfway to the sun!**

Approximately **6-8%** of packaged material sticks

About **0.03 km<sup>3</sup>** water loss/year

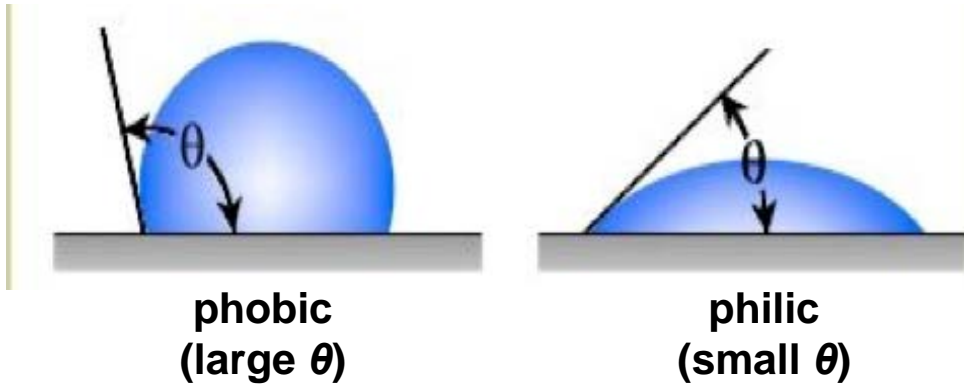
lake de l' Hongrin



# Solution: Superomniphobic surfaces

□ The way to **reduce product loss** is through the design of **superomniphobic** surfaces

➤ **Omniphobic** ( $\theta > 90^\circ$ ) and **superomniphobic** ( $\theta > 150^\circ$ ) are surfaces that repel all kinds of liquids



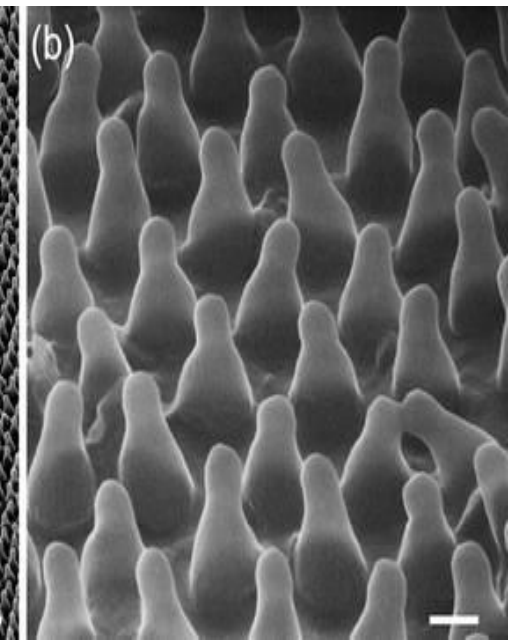
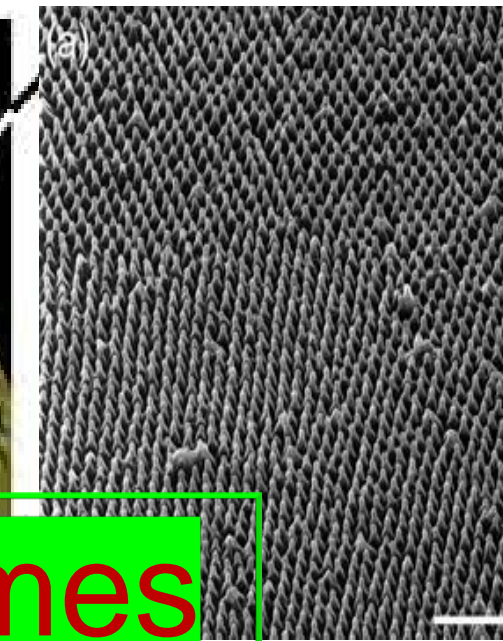
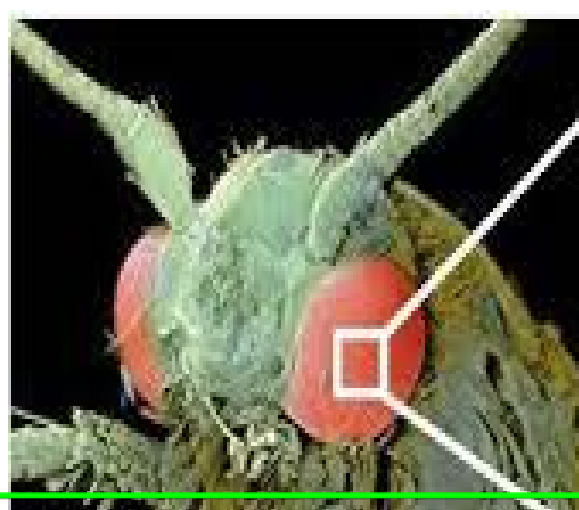
➤ Possibilities to induce omniphobicity include:

- **Chemical treatment** of surface (minor impact on wettability)<sup>1</sup>
- Treatment of the **surface topography** (more promising)

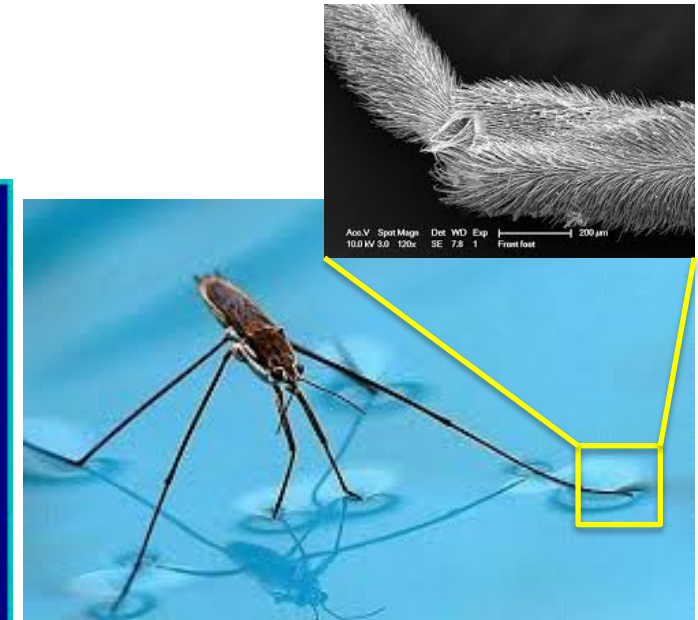
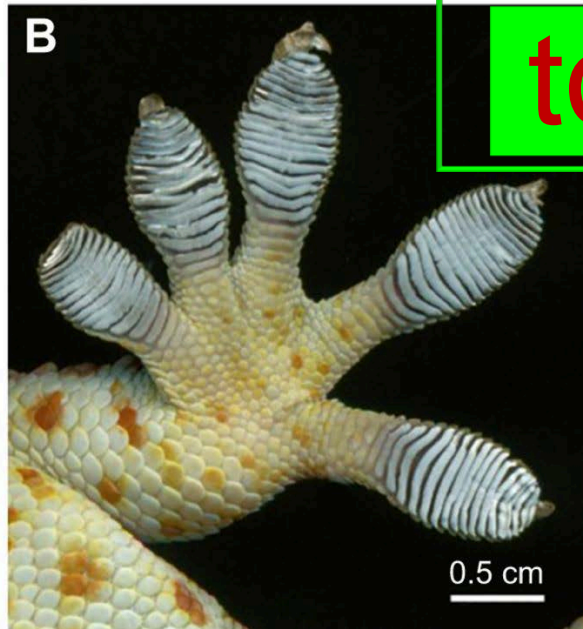
## □ Task:

➤ use **mathematical modelling** to quantify the relations between **surface topography and wetting**

1. Nishino, T et al. *Langmuir*, **1999**, 15, 4321-4323



Nature comes to the rescue!



Motivation

Solution

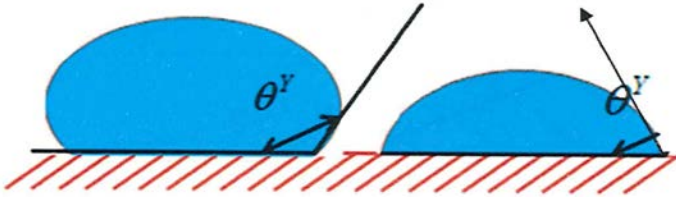
Implementation

Validation

Summary

# Solution: Bio-inspired surface topography manipulation

## 1. Young's Model<sup>1</sup> (1805)

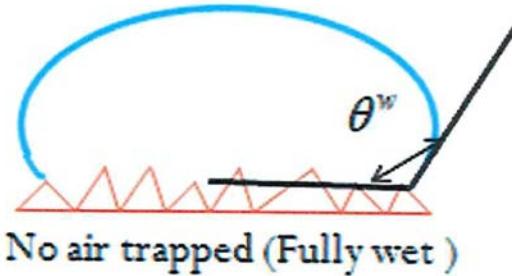


$$\cos \theta^Y = \frac{\gamma_s - \gamma_{sl}}{\gamma_l}$$

- Smooth surfaces 🙄
- Full wetting 🙄
- Unrealistic surface 🙄

1. Young, T. *Phil. Trans. R. Soc. Lond.* **1805**, 95, 65-87

## 2. Wenzel Model<sup>2</sup> (1936)

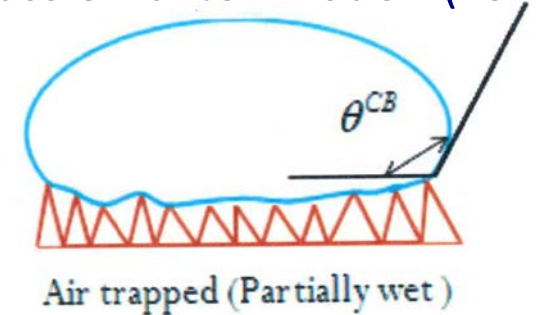


$$\cos \theta^W = \text{roughness} \cdot \cos \theta^Y$$

- Rough surfaces 👍
- Full wetting 🙄
- Unrealistic surface 🙄

2. Wenzel, R. N. *Industrial and engineering chemistry.* **1936**, 28(8)

## 3. Cassie-Baxter Model<sup>3</sup> (1944)



$$\cos \theta^{CB} = f_{sl} \cos \theta^Y - f_{la}$$

- Rough surfaces 👍
- Partial wetting 👍
- Realistic surface 👍
- Unrealistic interface 🙄

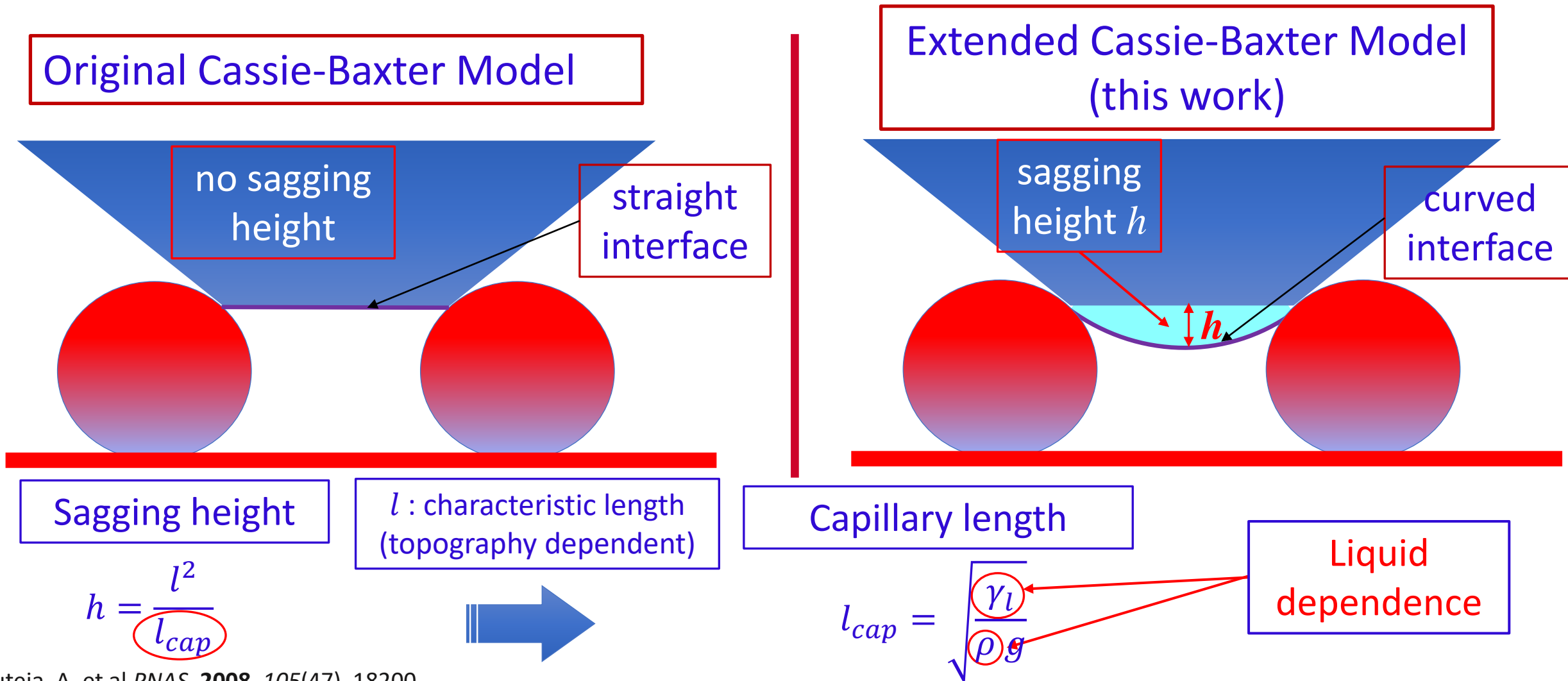
3. Cassie, A. B. D.; Baxter, S. *Wettability of porous surfaces.* **1944**

### □ It is evident that:

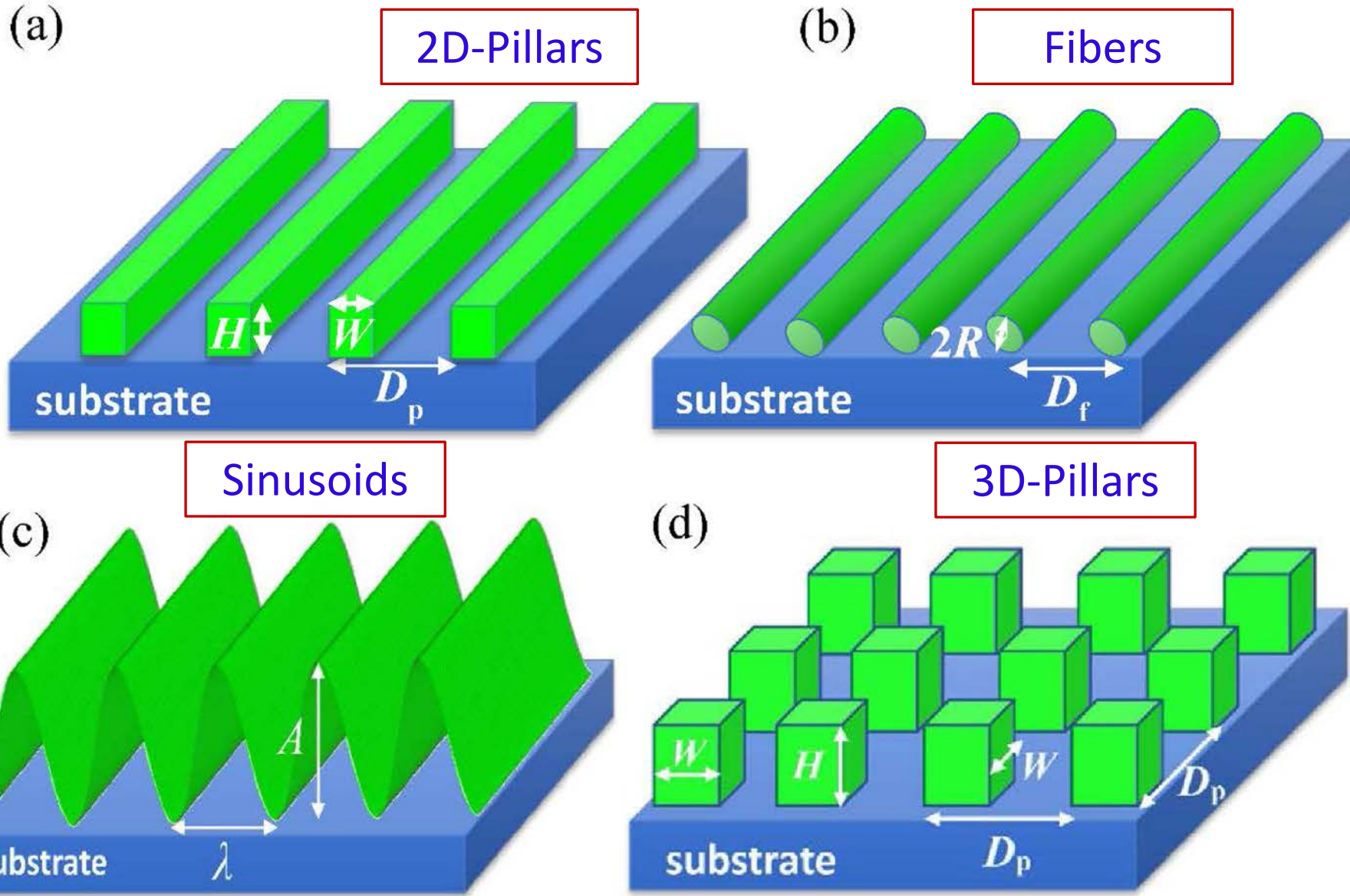
- the **Cassie-Baxter** model is the most realistic one accounting for **rough surfaces** and **partial wetting**
- However, **unrealistic interface**...

# Solution: Model details & innovation

- The liquid properties are expressed in terms of the **sagging height  $h^1$**



# Single-level surface topographies

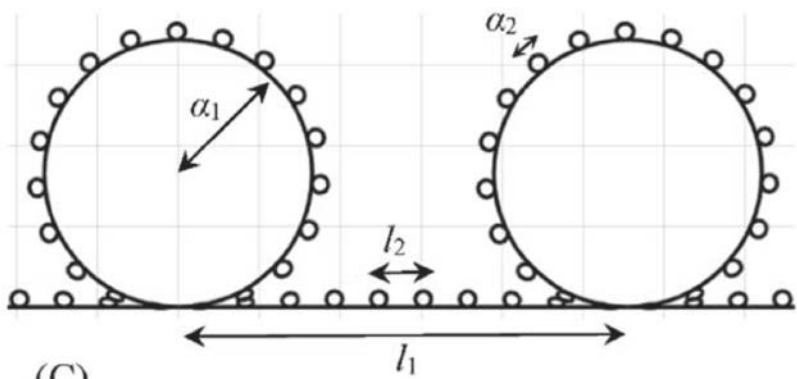


Topography	$l$
2D-Pillars	$D_p$
Fibers	$D_f$
Sinusoids	$\lambda$
3D-Pillars	$D_p$

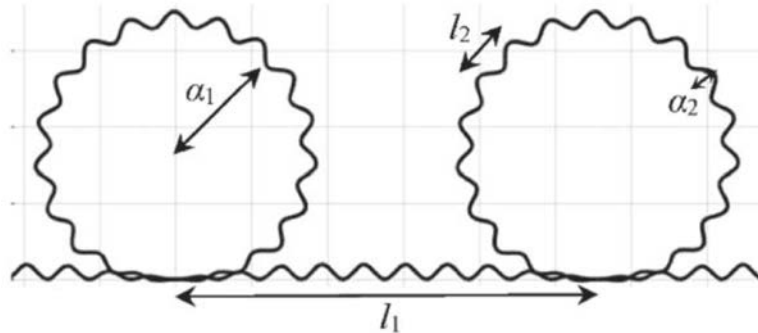


# Multi-level surface topographies

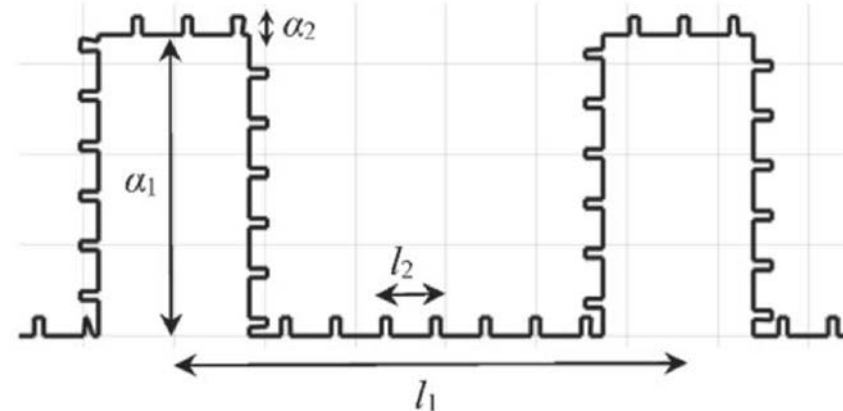
Fibers on Fibers



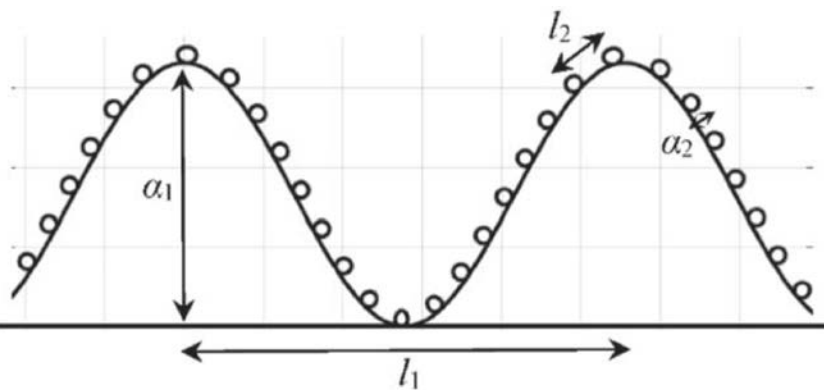
Sinusoids on Fibers



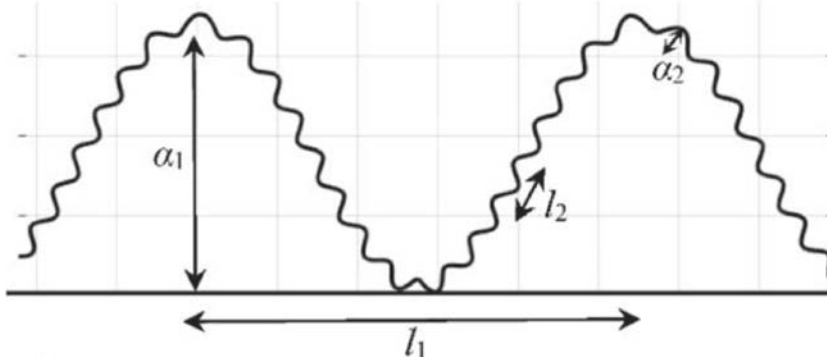
Pillars on Pillars



Fibers on Sinusoids



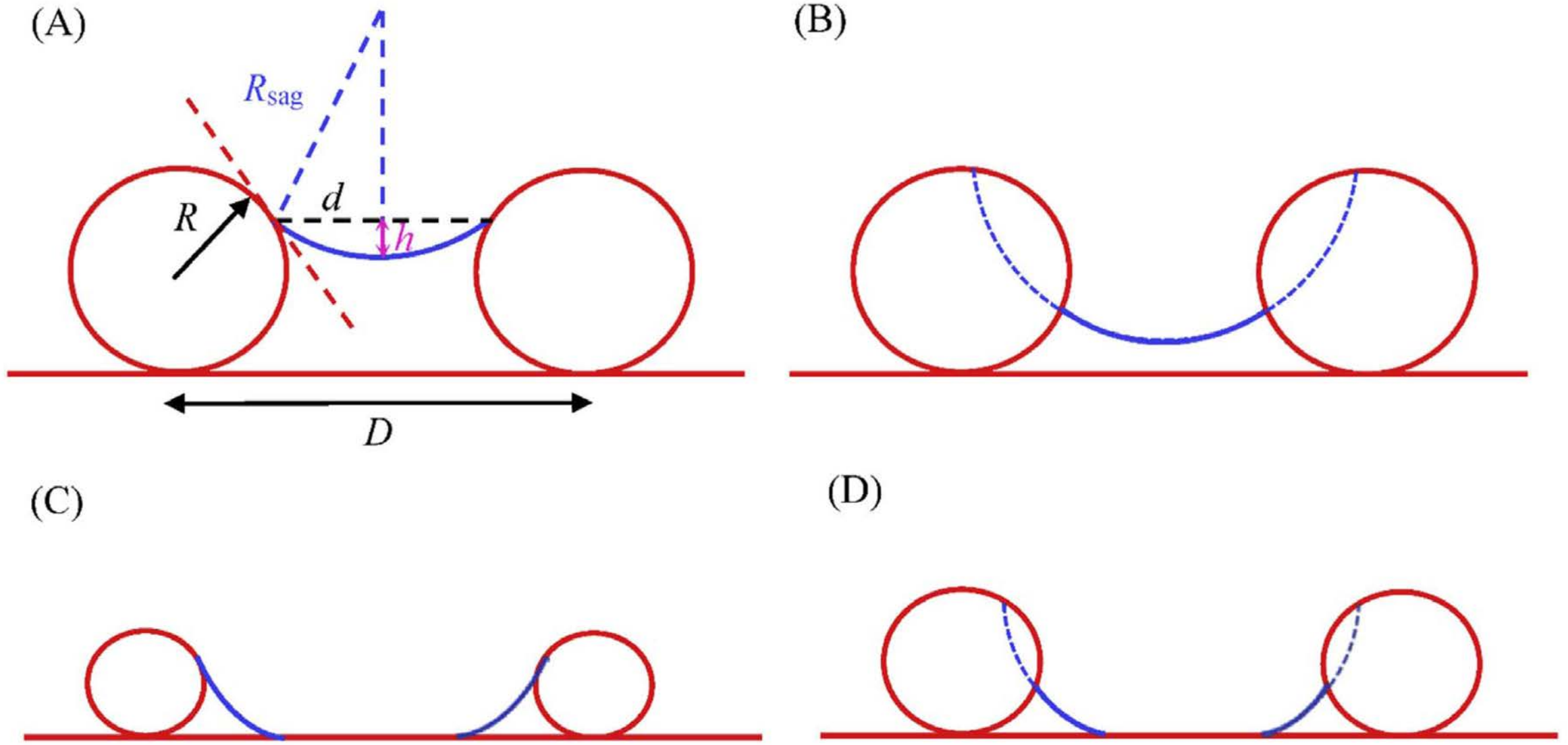
Sinusoids on Sinusoids



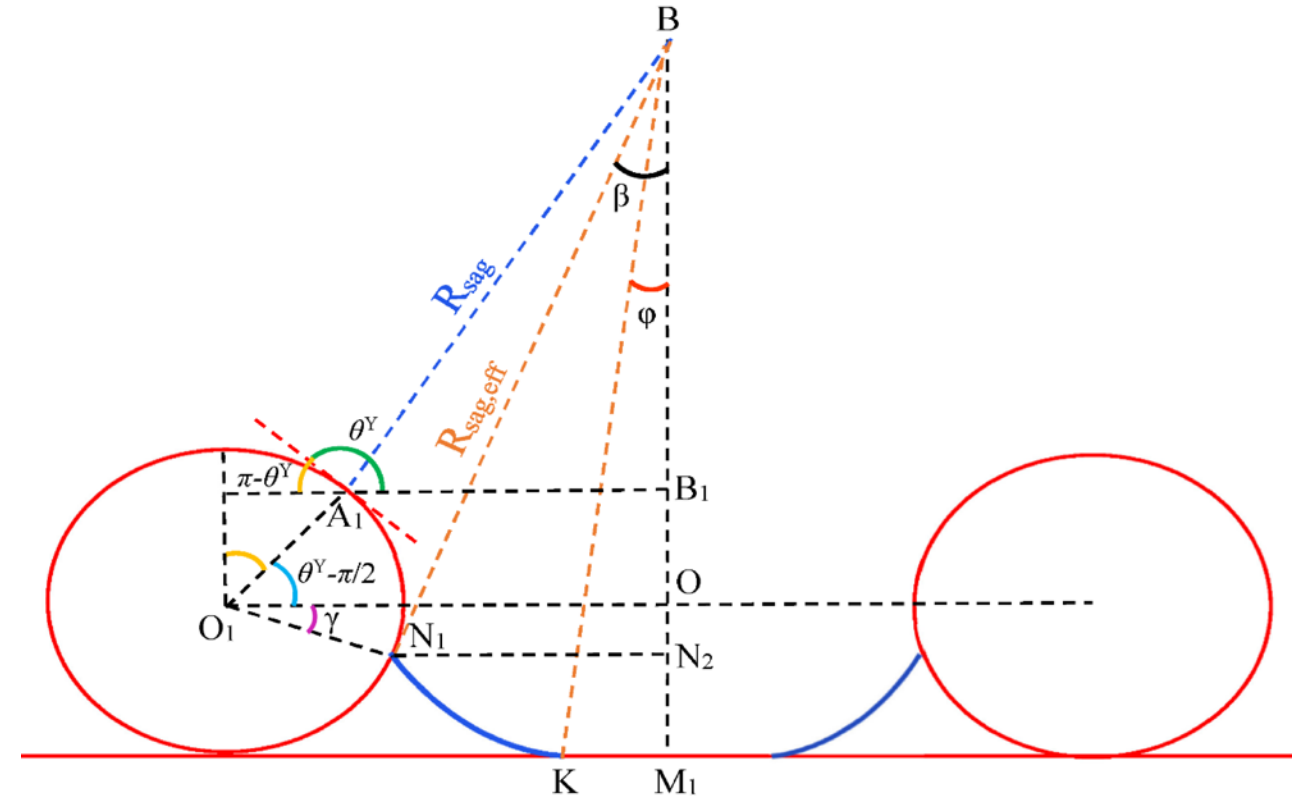
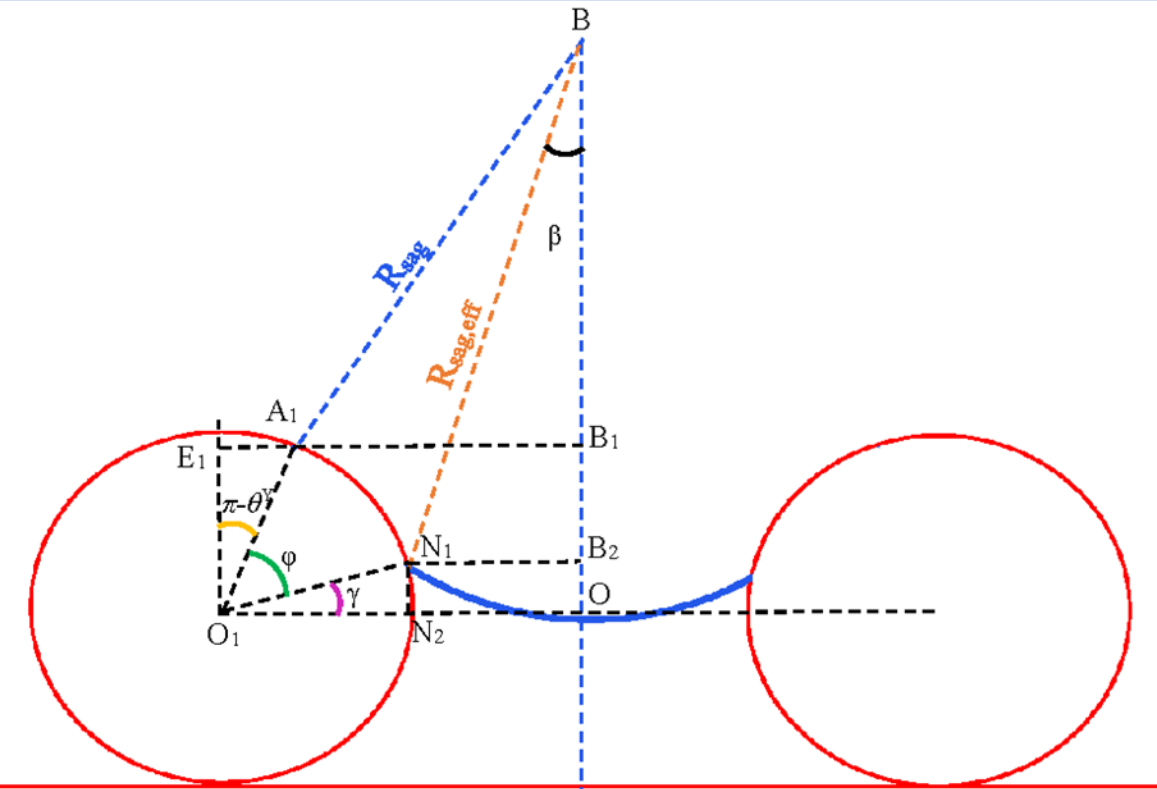
3x Sinusoids



# Fibers: Wetting scenarios



# Fibers: Mathematical derivations



$$f_{sl} = \frac{\text{actual wetted area}}{\text{total projected area}} = \frac{2R(\pi - \theta^Y)}{D} + \frac{2R\left(\theta^Y - \frac{\pi}{2} - \gamma\right)}{D}$$

$$f_{la} = \frac{2\beta R_{sag,eff}}{D} = \frac{2R_{sag,eff}}{D} \arccos \left[ \frac{(\sqrt{R_{sag,0}^2 - d^2} - R \cos \theta^Y - R \sin \gamma)}{R_{sag,eff}} \right]$$

$$f_{sl} = \frac{\text{actual wetted area}}{\text{total projected area}} = \frac{2R(\pi - \theta^Y)}{D} + \frac{2R_{sag}}{D} \sqrt{1 - \cos^2 \phi}$$

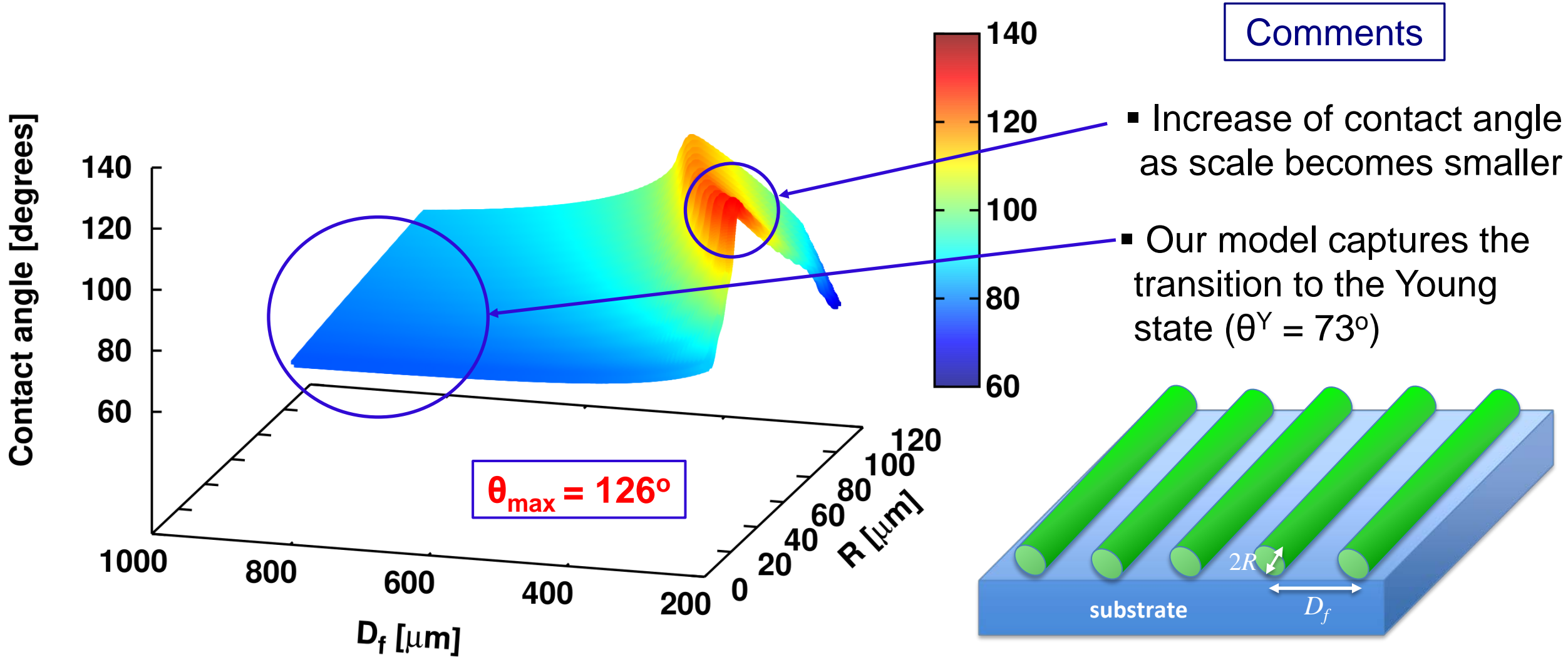
Lempesis et al., 2020

# Model input

Parameter	Value
liquid	Water
surface	LDPE
<i>Young's angle</i> $\theta^Y$	73°
liquid density $\rho$	997 kg/m <sup>3</sup>
liquid surface tension $\gamma_l$	72.8 mN/m

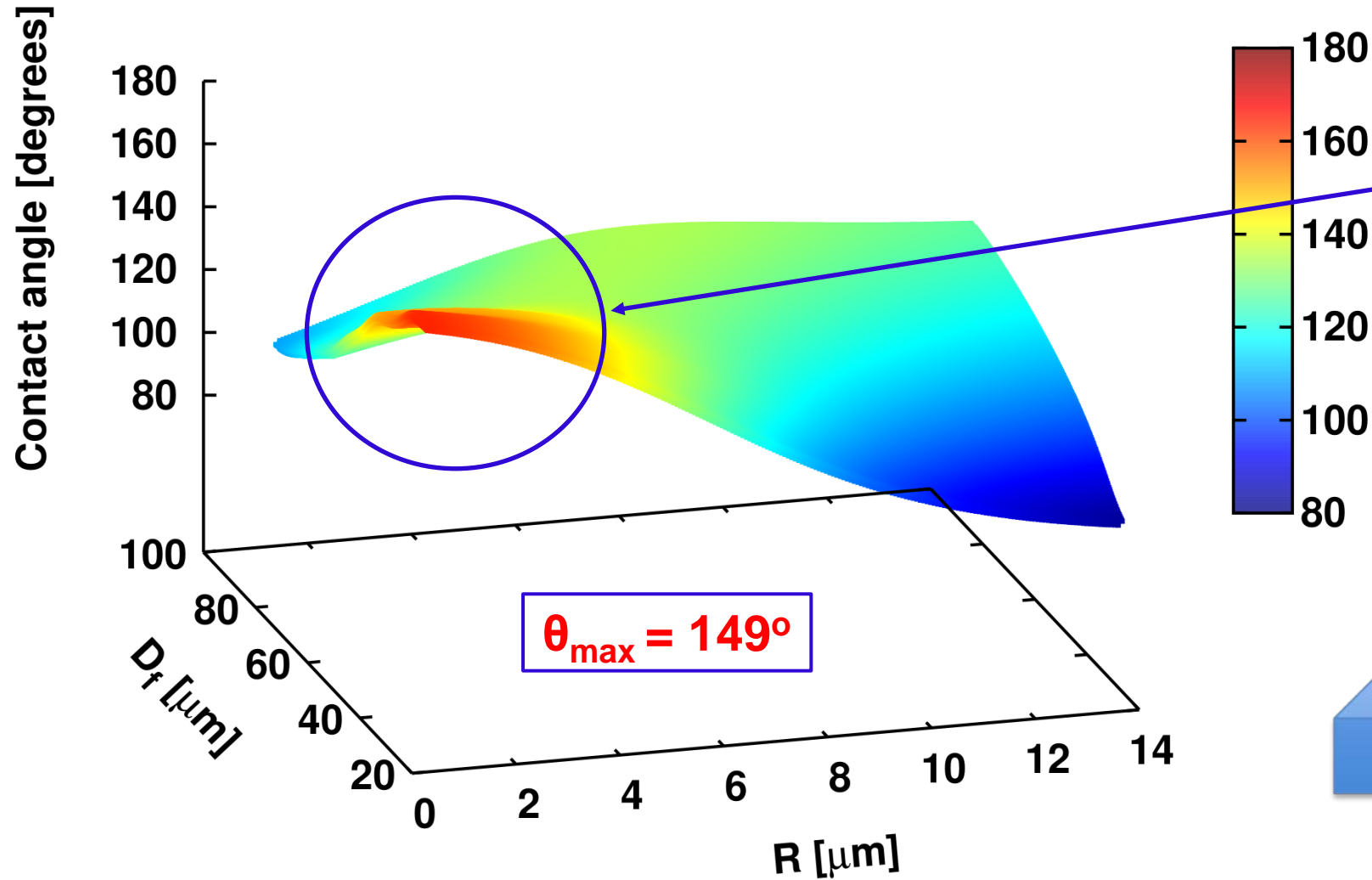
Lempesis et al., 2020

# Fibers: Model output



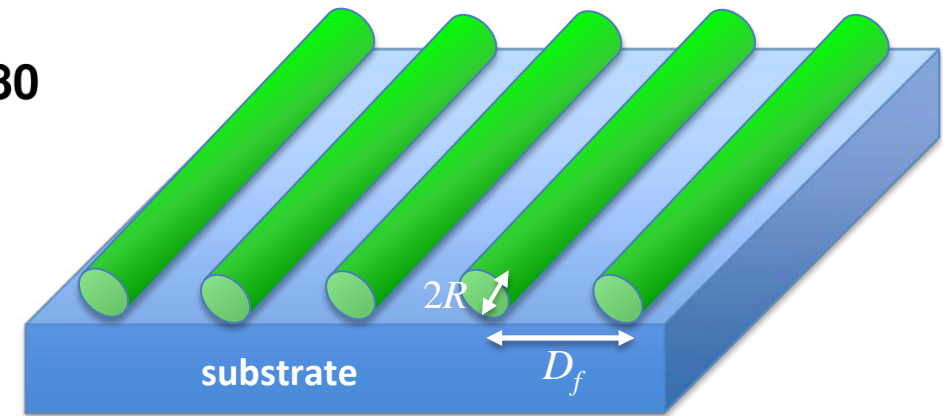
Lempesis et al., 2020

# Fibers: Scale effect

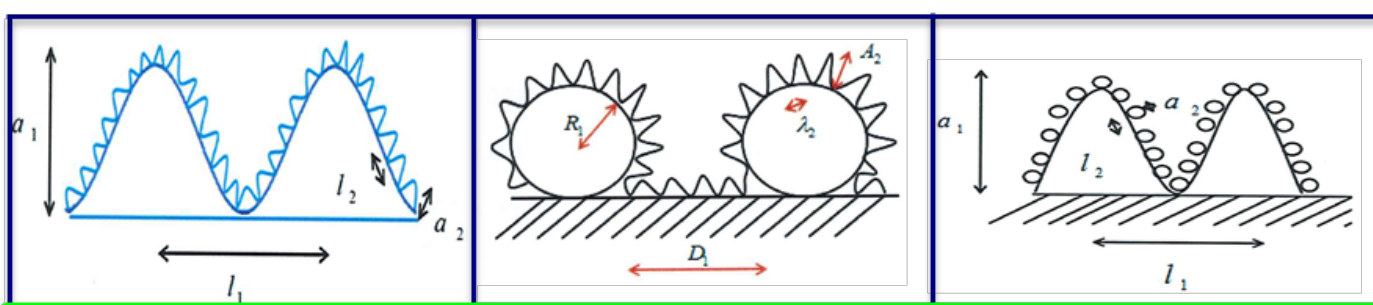


## Comments

- As fiber scale drops, phobicity increases considerably
- Fabrication of **nanoscale** patterns is a formidable technological challenge

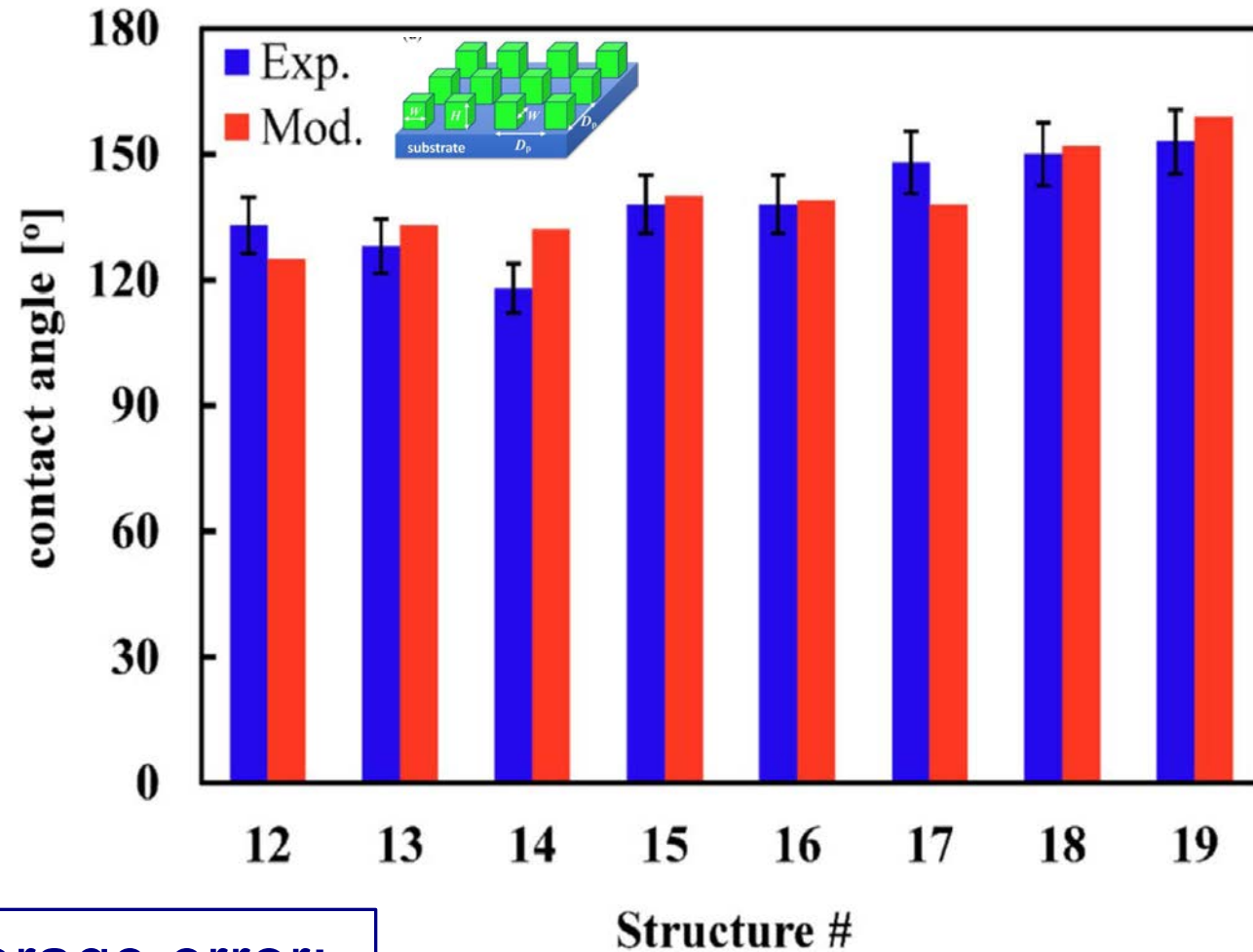
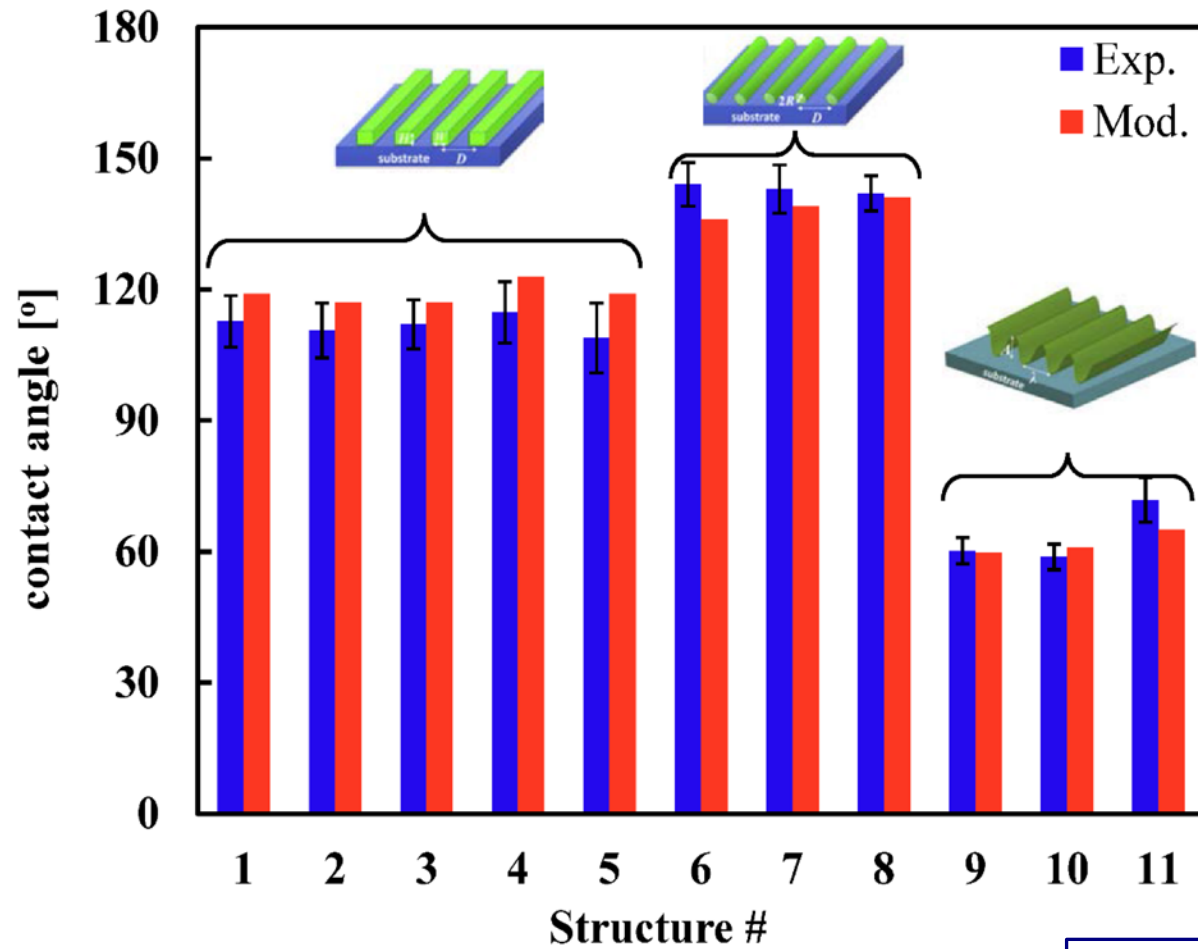


Lempesis et al., 2020



	Two-level topography			Single-level topography
Ext. Cassie/Baxter	Sine on Sine	Sine on Fibers	Fibers on Sine	Sine
Max. Contact Angle [°]	140	149	<b>162</b>	100
Scale1 [μm] (coarse scale)	$A_1 = 161$	$R = 28$	$A = 161$	$A = 81$
	$\lambda_1 = 252$	$D_f = 217$	$\lambda = 252$	$\lambda = 126$
Scale2 [μm] (fine scale)	$A_2 = 16$	$A = 32$	$R = 7$	n/a
	$\lambda_2 = 25$	$\lambda = 50$	$D_f = 28$	n/a

# Model validation: single-level topographies

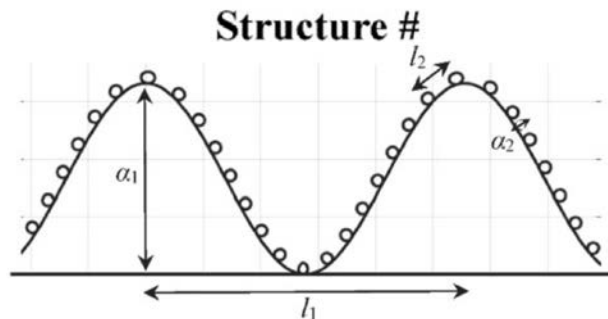
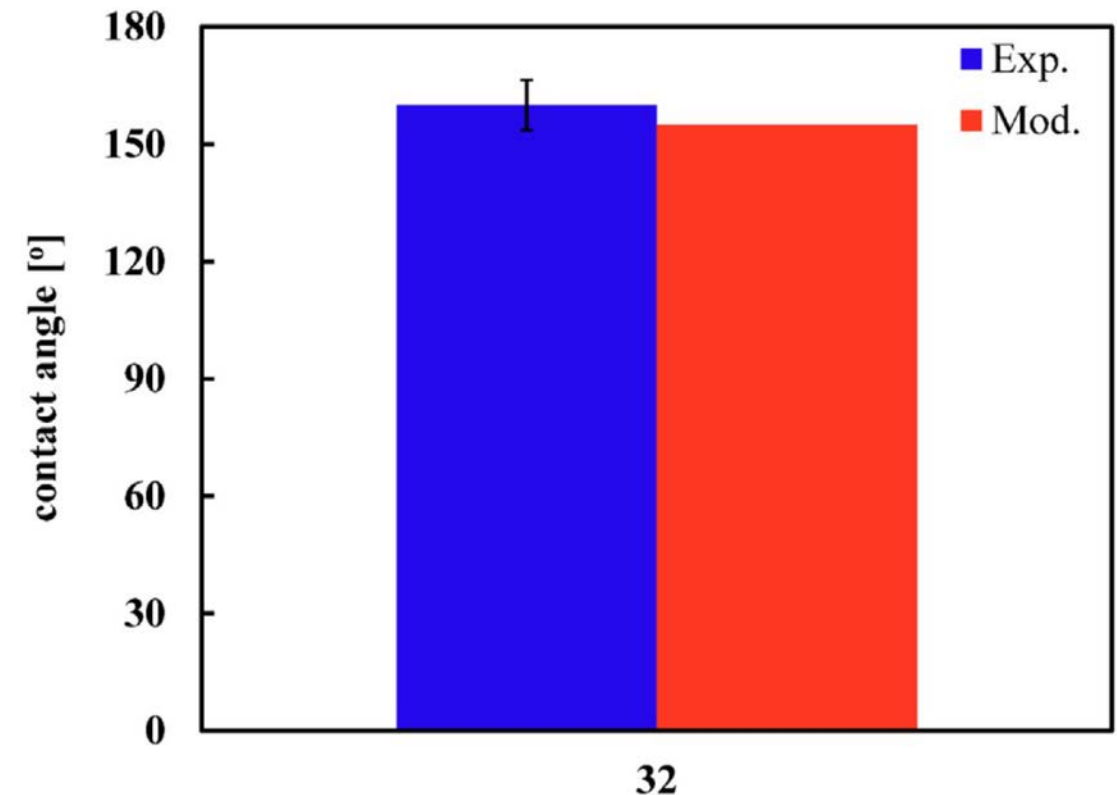
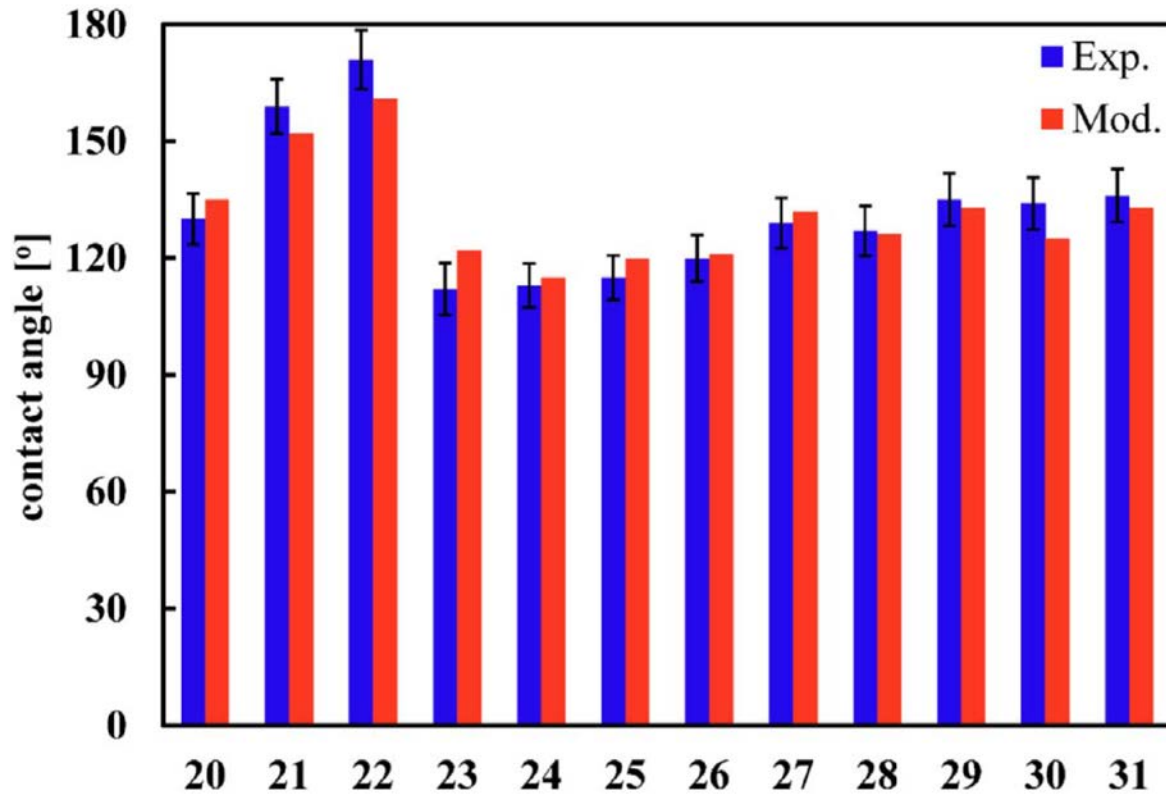


Average error:  
4.6 %

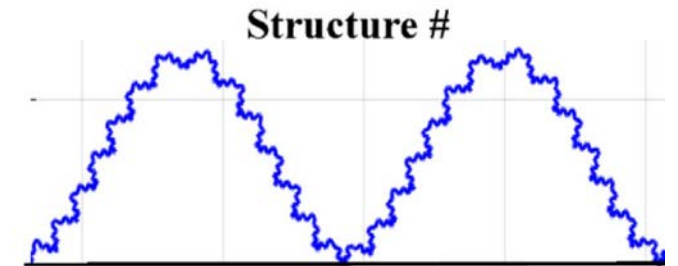
Lempesis et al., 2021



# Model validation: multi-level topographies



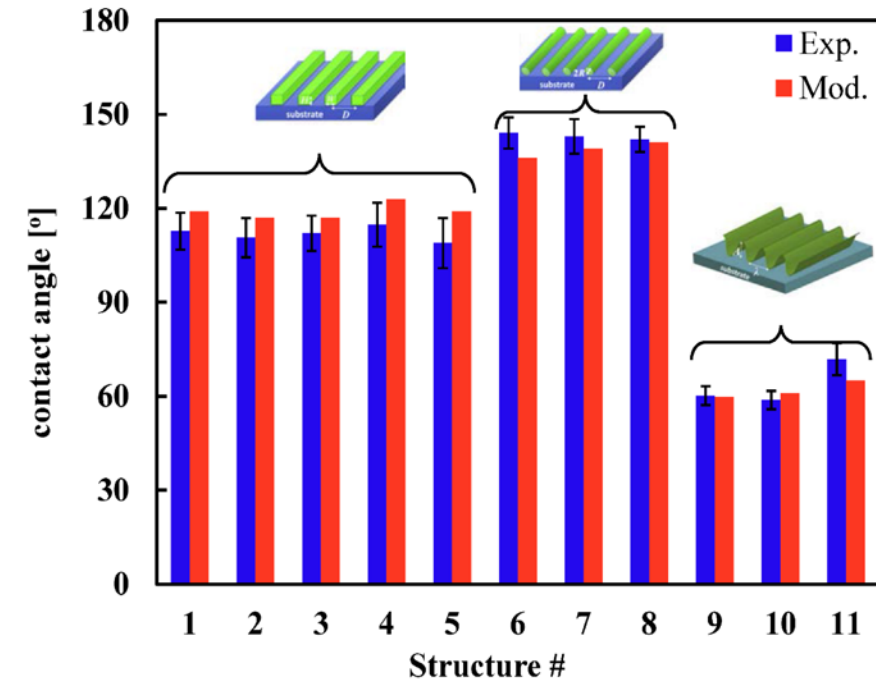
Average error:  
3.5 %



Lempesis et al., 2021

# Summary and next steps

- An extended Cassie-Baxter model with realistic interfaces was developed for single- and multi-level topographies
- Our model captures the transitions to the Wenzel and Young states and length scale effect
- Model results deviated on average from exp. data by (~4%)
- Addition of a 2<sup>nd</sup> level almost doubled the contact angle, while a 3<sup>rd</sup> level brought about an additional 12.5% increase



- Creation of a user-friendly Graphical User Interface (GUI)
- Extension of formalism to more surface topography types
- Modeling the wetting behavior of moving droplets (self-cleaning)

# Acknowledgements

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**IKY**



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